



nonsmooth structured control design

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outline

motivation

nonsmooth optimization

controller design

conclusion

context

- challenging **practical** design problems:
 - reduced- and fixed-order synthesis
 - structured and fixed-architecture synthesis problems
 - general robust control with uncertain and/or nonlinear components
 - simultaneous model/controller design, multimodel control
 - multi-objective frequency- and time-domain designs
 - combinations of the above, etc
- classical design methods (Riccati, LMI) fail on sizeable plants.
- D-K schemes and heuristic methods (homotopy, . . .) not satisfactory
- solutions based on LMI relaxations often very conservative

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an illustrative example

Boeing 767 at flutter condition

stabilization with static output feedback $u = Ky$:

$$\begin{bmatrix} \dot{x} \\ y \end{bmatrix} = \begin{bmatrix} A & B \\ C & 0 \end{bmatrix} \begin{bmatrix} x \\ u \end{bmatrix}$$

$$A = 55 \times 55 \quad B = 55 \times 2 \quad C = 2 \times 55 \quad K = 2 \times 2$$

- BMI: $(A + BKC)^T P + P(A + BKC) \prec 0$ et $P = P^T \succ 0$
 \Rightarrow 1544 variables most of them (1540) for Lyapunov matrix P
- $\min_K \alpha(A + BKC)$ where $\alpha \triangleq \max_i \operatorname{Re} \lambda_i$ is spectral abscissa
 \Rightarrow 4 variables : controller parameters

\Rightarrow recast controller design as a nonsmooth program

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controller design as nonsmooth (minimax) optimization

- stabilization

$$\min_K \max_i \operatorname{Re} \lambda_i(A + BKC)$$

- H_∞ synthesis

$$\min_K \max_{\omega \in [0, +\infty]} \max_i \sigma_i(T_{w \rightarrow z}(K, j\omega))$$

- time-domain design

$$\min_K \max_{t \in [0, +\infty]} \max \left\{ (z(K, t) - z_{\max}(t))^+, (z_{\min}(t) - z(K, t))^+ \right\}$$

- generic BMI problem

$$\min_x \max_i \lambda_i \left(A_0 + \sum_k x_k A_k + \sum_k \sum_l x_k x_l B_{kl} \right)$$

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controller design as nonsmooth optimization

- these optimization problems are nonsmooth and/or nonconvex
- special **composite** structure

$$\max_{x \in X} \lambda_1 \circ T(K, x)$$

where $\max_{x \in X} \lambda_1$ is convex and $T(K, x)$ differentiable wrt. $K, \forall x$

Clarke subdifferential

Clarke regularity \Rightarrow specialized and efficient techniques can be developed

- **directly** formulated in controller parameter space (no Lyapunov variables)
- **flexible**: to handle controller structural constraints
- **efficient**: to handle large control problems

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subdifferential and subgradients

nonsmooth minimax optimization problems of the form

$$\boxed{
 \begin{array}{c}
 \min_K \max_{x \in X} f(K, x) \\
 \underbrace{\hspace{10em}} \\
 \triangleq f_\infty(K)
 \end{array}
 }$$

X stands for:

- a **finite set** of indices : $X = \{1, \dots, q\}$

$$\min_K \max_i \operatorname{Re} \lambda_i(A + BKC)$$

- a **time- or frequency-domain closed interval** :
 $X = [0, +\infty]$, $X = [0, t_{max}]$, $X = [\omega_1, \omega_2]$, \dots

$$\min_K \max_{t \in [0, +\infty]} (z(K, t) - z_{max}(t))$$

- **double max** : $\min_K \max_{\omega \in [0, +\infty]} \max_i \sigma_i(T_{w \rightarrow z}(K, j\omega))$.

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$$\boxed{\min_K \max_{x \in X} \underbrace{f(K, x)}_{\triangleq f_\infty(K)}}$$

assume (for simplicity) that f is continuous and $K \mapsto f(K, x)$ is \mathcal{C}^1 $\forall x \in X$.

then f_∞ is loc. Lipschitz and admits a **Clarke subdifferential** $\forall K$:

$$\boxed{\partial f_\infty(K) = \text{co}_{x \in \hat{X}(K)} \nabla_K f(K, x)}$$

where $\hat{X}(K) \triangleq \{x \in X : f_\infty(K) = f(x, K)\}$ **active set**.
 vectors $\phi \in \partial f_\infty(K)$ are **Clarke subgradients** of f_∞ at K .

nonsmooth optimality condition

Theorem ([Clarke, 1983])

K^* is a local minimum of $f_\infty \implies 0 \in \partial f_\infty(K^*)$

- define **optimality function** θ to check whether $0 \in \partial f_\infty(K)$ satisfied at K .
- if not, find a **descent step** $H(K)$ for $f_\infty(K)$, i.e. $\exists t_K > 0$ such that, for all $t \in (0, t_K]$

$$f_\infty(K + tH(K)) < f_\infty(K)$$

- **steepest descent:**

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- **steepest descent:**

$$H(K) \triangleq -\arg \underbrace{\min_H \max_{\phi \in \partial f_\infty(K)} \langle \phi, H \rangle + \frac{1}{2} \|H\|^2}_{\triangleq \theta_1(K)}$$

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$\implies K \mapsto H(K)$ **not continuous ! convergence problem.**

nonsmooth descent direction

$$H(K) \triangleq \arg \min_H \max_{x \in \hat{X}_e(K)} \underbrace{f(K, x) + \langle \nabla_K f(K, x), H \rangle + \frac{1}{2} \delta \|H\|^2}_{\text{1st-order quadratic local model of } f(\cdot, x) \text{ at } K} - f_\infty(K)$$

$\delta > 0$, $\hat{X}_e(K) \supset \hat{X}(K)$, finite extension of active set

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Proposition ([Apkarian and Noll, 2006-I])

- $\theta(K) \leq 0$ and $\theta(K) = 0 \iff 0 \in \partial f_\infty(K)$
 $\theta(K)$ **criticality measure** of K for f_∞
- $\theta(K)$ **termination test and (local) optimality certificate**
- $K \mapsto \theta(K)$ **continuous**
- $f'_\infty(K; H(K)) \leq \theta(K) - \frac{1}{2\delta} \|H(K)\|^2 < 0$
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nonsmooth optimality condition

- primal QP problem

$$\underbrace{\min_H \max_{x \in \hat{X}_e(K)} f(K, x) + \langle \nabla_K f(K, x), H \rangle + \frac{1}{2} \delta \|H\|^2 - f_\infty(K)}_{\text{optimality function } \theta(K)}$$

- dual QP problem (equivalent)

$$\theta(K) = - \min_{\substack{\tau_x \geq 0 \\ \sum \tau_x = 1}} \sum_{x \in \hat{X}_e(K)} \tau_x (f_\infty(K) - f(K, x)) + \frac{1}{2\delta} \left\| \sum_{x \in \hat{X}_e(K)} \tau_x \nabla_K f(K, x) \right\|^2$$

with

$$H(K) = -\frac{1}{\delta} \sum_{x \in \hat{X}_e(K)} \tau_x^* \nabla_K f(K, x)$$

- select primal or dual with smaller dimension

nonsmooth optimality condition

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nonsmooth descent algorithm

Algorithm ([Apkarian and Noll, 2006-I, Polak, 1997])

set $\beta \in (0, 1)$, $\delta > 0$, $\varepsilon_\theta > 0$.

Initialize with controller K_0 .

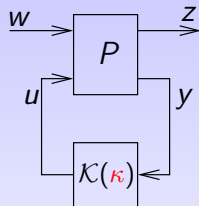
- 1 set counter $l \leftarrow 0$
- 2 find **active set** $\hat{X}(K_l)$.
- 3 build a **finite extension** $\hat{X}_e(K_l)$.
- 4 compute the **optimality function value** (convex QP) $\theta(K_l)$ and the **search direction** $H(K_l)$.
- 5 if $|\theta(K_l)| < \varepsilon_\theta$ (criticality test), **stop**.
else compute the **step-size** t_l such that

$$f_\infty(K_l + t_l H(K_l)) - f_\infty(K_l) \leq t_l \beta \theta(K_l)$$

- 6 set $K_{l+1} \leftarrow K_l + t_l H(K_l)$, $l \leftarrow l + 1$ and go to step 2.

synthesis formulation

$$P(s) \left\{ \begin{bmatrix} \dot{x} \\ z \\ y \end{bmatrix} = \begin{bmatrix} A & B_1 & B_2 \\ C_1 & D_{11} & D_{12} \\ C_2 & D_{21} & 0 \end{bmatrix} \begin{bmatrix} x \\ w \\ u \end{bmatrix} \right.$$



- $\mathcal{K}(\kappa)$ defines controller structure
- find κ free parameters to achieve stability, frequency- or time-domain constraints

structured controller design

controller structural constraints

$\mathcal{K}(\kappa)$ with $\kappa \in \mathbb{R}^q$ vector of **free controller parameters**

structured controller design

controller structural constraints

$\mathcal{K}(\kappa)$ with $\kappa \in \mathbb{R}^q$ vector of **free controller parameters**

PID control ($m_2 \times m_2$)

$$\mathcal{K}(\kappa) = \left[\begin{array}{cc|c} 0 & 0 & R_i \\ 0 & -\tau I_{m_2} & R_d \\ \hline I_{m_2} & I_{m_2} & D_K \end{array} \right]$$

such that $K(s) = D_K + \frac{R_i}{s} + \frac{R_d}{s+\tau}$.

here $\kappa = [\tau \quad (\text{vec } R_i)^T \quad (\text{vec } R_d)^T \quad (\text{vec } D_K)^T]^T$.

structured controller design

controller structural constraints

$\mathcal{K}(\kappa)$ with $\kappa \in \mathbb{R}^q$ vector of free controller parameters

observer-based control (LQG)

$$\mathcal{K}(\kappa) = \left[\begin{array}{c|c} A - B_2 K_c - K_f C_2 & K_f \\ \hline -K_c & 0 \end{array} \right]$$

K_f state estimator gain,

K_c state feedback gain.

$$\kappa = [(\text{vec } K_f)^T \quad (\text{vec } K_c)^T]^T$$

structured controller design

controller structural constraints

$\mathcal{K}(\kappa)$ with $\kappa \in \mathbb{R}^q$ vector of free controller parameters

fractional representations

$$K(s, \kappa) = (N_m s^m + \dots + N_0)(D_n s^n + \dots + D_0)^{-1}$$

N_j numerator coefficients

D_j denominator coefficients

$$\kappa = [\dots (\text{vec } N_j)^T \dots (\text{vec } D_j)^T \dots]^T$$

etc

any differentiable possibly nonlinear $\mathcal{K}(\kappa)$

structured controller design

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$\mathcal{K}(\kappa)$ with $\kappa \in \mathbb{R}^q$ vector of **free controller parameters**

the nonsmooth problem becomes

$$\min_{\kappa \in \mathbb{R}^q} \max_{x \in X} \underbrace{f(\mathcal{K}(\kappa), x)}_{f_\infty(\mathcal{K}(\kappa))}$$

chain rule for subdifferentials with $\mathcal{K} \in \mathcal{C}^1(\mathbb{R}^q)$:

$$\partial(f_\infty \circ \mathcal{K})(\kappa) = \mathcal{K}'(\kappa)^* [\partial f_\infty(\mathcal{K}(\kappa))]$$

subgradients $\psi = J_{\mathcal{K}}(\kappa)^T \phi$

where $J_{\mathcal{K}}$ Jacobian matrix of \mathcal{K} , and $\phi \in \partial f_\infty(\mathcal{K}(\kappa))$

stabilization

$$\min_K \max_i \underbrace{\operatorname{Re} \lambda_i(A + B_2 K C_2)}_{f_\infty(K)}$$

minimize spectral abscissa $\alpha \triangleq \max_i \operatorname{Re} \lambda_i$.

- **active set** of closed-loop eigenvalues indices :

$$\hat{X}(K) = \{i = 1 \dots n : \operatorname{Re} \lambda_i(A + B_2 K C_2) = \alpha(A + B_2 K C_2)\}$$

extended set $\hat{X}_e(K) \supset \hat{X}(K)$ with neighboring eigenvalues.

- working assumption: all the closed-loop eigenvalues λ_i , $i \in \hat{X}_e(K)$, are **simple**.
- subgradients $\phi(K) \in \partial f_\infty(K)$:

$$\phi(K) = \sum_{i \in \hat{X}(K)} \left(\tau_i \operatorname{Re} (C_2 v_i u_i^H B_2)^T \right)$$

- v_i right eigenvector associated with λ_i
- u_i^H left eigenvector associated with λ_i
- $\tau_i \geq 0$ and $\sum_{i \in \hat{X}(K)} \tau_i = 1$
- stop before convergence if $\alpha(A + B_2 K C_2) < 0$ (K stabilizing).

stabilization

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- working assumption: all the closed-loop eigenvalues λ_i , $i \in \hat{X}_e(K)$, are **simple**.
- subgradients $\phi(K) \in \partial f_\infty(K)$:

$$\phi(K) = \sum_{i \in \hat{X}(K)} \left(\tau_i \operatorname{Re} (C_2 v_i u_i^H B_2)^T \right)$$

- v_i right eigenvector associated with λ_i
- u_i^H left eigenvector associated with λ_i
- $\tau_i \geq 0$ and $\sum_{i \in \hat{X}(K)} \tau_i = 1$
- stop before convergence if $\alpha(A + B_2 K C_2) < 0$ (K stabilizing).

stabilization

$$\min_K \max_i \underbrace{\operatorname{Re} \lambda_i(A + B_2 K C_2)}_{f_\infty(K)}$$

minimize spectral abscissa $\alpha \triangleq \max_i \operatorname{Re} \lambda_i$.

- **active set** of closed-loop eigenvalues indices :

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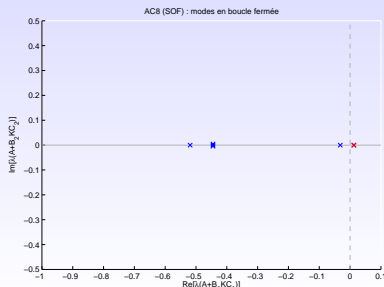
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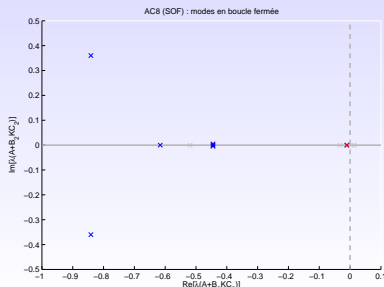
examples from Leibfritz's collection

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| AC8 ($n_K = 1$) | (9, 1, 5) | 5 | 0.2 | 17 | 0.4 | $-4.45 \cdot 10^{-1}$ | $-5.01 \cdot 10^{-27}$ |
| HE2 (SOF) | (4, 2, 1) | 1 | < 0.1 | 216 | 2.3 | $-2.39 \cdot 10^{-1}$ | $-9.77 \cdot 10^{-6}$ |
| HE2 ($n_K = 1$) | (4, 2, 1) | 1 | < 0.1 | (28) | 0.7 | $-2.31 \cdot 10^{-1}$ | -1.53 |
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| REA2 (PID) | (4, 2, 2) | 1 | < 0.1 | (19) | 0.6 | -1.27 | $-1.4 \cdot 10^{-1}$ |
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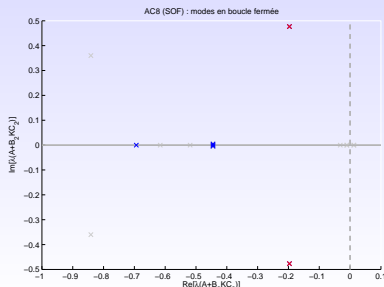
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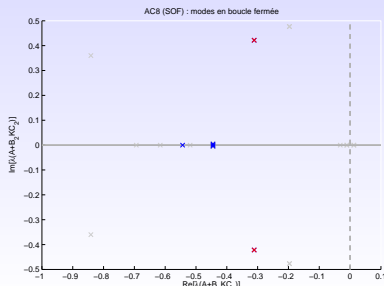
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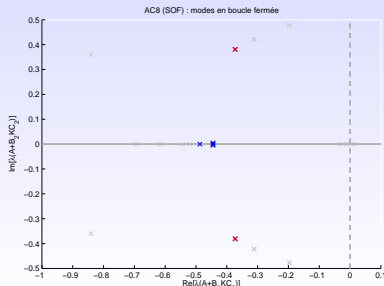
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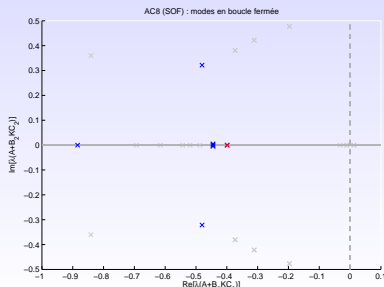
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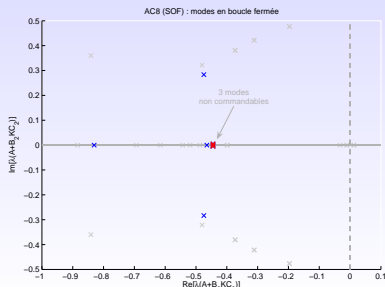
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examples from Leibfritz's collection

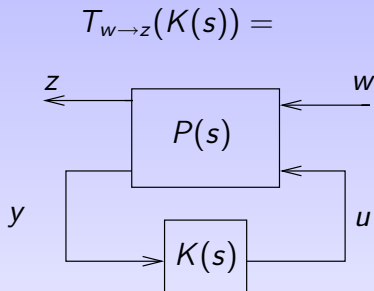
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H_∞ synthesis

$$\min_K \max_{\omega \in [0, +\infty]} \max_i \sigma_i(T_{w \rightarrow z}(K, j\omega))$$

$= \|T_{w \rightarrow z}(K, \cdot)\|_\infty = f_\infty(K)$



$$T_{w \rightarrow z}(K(s)) := P_{11} + P_{12}K(I - P_{22}K)^{-1}P_{21}$$

- composite $\|\cdot\|_\infty \circ T_{w \rightarrow z}$ is **Clarke regular as a composite of convex and differentiable maps**
- \Rightarrow exhaustive description of subdifferential

$$\partial(\|\cdot\|_\infty \circ T_{w \rightarrow z})(K)$$

Clarke subdifferential of H_∞ norm

with standard notations define closed-loop data

$$\begin{aligned} \mathcal{A}(K) &:= A + B_2 K C_2, & \mathcal{B}(K) &:= B_1 + B_2 K D_{21}, \\ \mathcal{C}(K) &:= C_1 + D_{12} K C_2, & \mathcal{D}(K) &:= D_{11} + D_{12} K D_{21}, \end{aligned}$$

introduce notation

$$\begin{aligned} \begin{bmatrix} T_{w \rightarrow z}(K, s) & G_{12}(K, s) \\ G_{21}(K, s) & \star \end{bmatrix} &:= \\ \begin{bmatrix} \mathcal{C}(K) \\ C_2 \end{bmatrix} (sI - \mathcal{A}(K))^{-1} \begin{bmatrix} \mathcal{B}(K) & B_2 \end{bmatrix} &+ \begin{bmatrix} \mathcal{D}(K) & D_{12} \\ D_{21} & \star \end{bmatrix}. \end{aligned}$$

- use appropriate plant augmentation if dynamic controller

Clarke subdifferential of H_∞ norm

Apkarian & Noll, 2006, [Apkarian and Noll, 2006-I]

subdif. is convex-compact set of subgradients Φ_Y 's

$$\frac{\sum_{\nu=1}^p \operatorname{Re} \{ G_{21}(K, j\omega_\nu) T_{w \rightarrow z}(K, j\omega_\nu)^H Q_\nu Y_\nu Q_\nu^H G_{12}(K, j\omega_\nu) \}^T}{\|T_{w \rightarrow z}(K)\|_\infty}$$

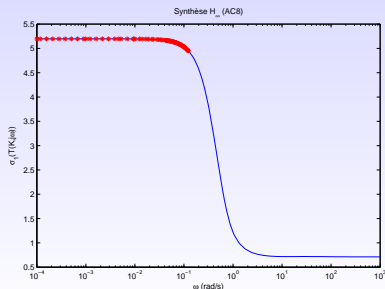
- ω_ν are active (peak) frequencies at K
- $Y := (Y_1, \dots, Y_p)$ ranges over spectraplex (convex)

$$\{ Y = (Y_1, \dots, Y_p) : Y_i = Y_i^H, \succeq 0, \sum_{\nu=1}^p \operatorname{Tr}(Y_\nu) = 1 \}$$

- use chain rule $\mathcal{K}(\kappa)'^* \partial(\|\cdot\|_\infty \circ T_{w \rightarrow z})(\mathcal{K}(\kappa))$ if structured controllers

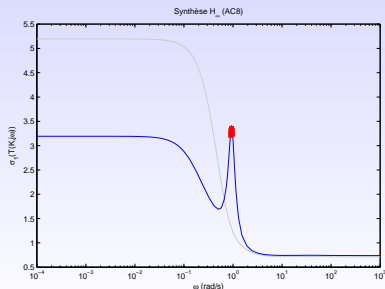
examples from Leibfritz's collection

| problem | (n, m, p) | order | iter | cpu (sec.) | nonsmooth H_∞ | H_∞ AL | FW | H_∞ full |
|---------|-------------|-------|------|------------|----------------------|---------------|-------|-----------------|
| AC8 | (9, 1, 5) | 0 | 20 | 45 | 2.005 | 2.02 | 2.612 | 1.62 |
| HE1 | (4, 2, 1) | 0 | 4 | 7 | 0.154 | 0.157 | 0.215 | 0.073 |
| REA2 | (4, 2, 2) | 0 | 31 | 51 | 1.192 | 1.155 | 1.263 | 1.141 |
| AC10 | (55, 2, 2) | 0 | 15 | 294 | 13.11 | * | * | 3.23 |
| AC10 | (55, 2, 2) | 1 | 46 | 408 | 10.21 | * | * | 3.23 |
| BDT2 | (82, 4, 4) | 0 | 44 | 1501 | 0.8364 | * | * | 0.2340 |
| HF1 | (130, 1, 2) | 0 | 11 | 1112 | 0.447 | * | * | 0.447 |
| CM4 | (240, 1, 2) | 0 | 2 | 3052 | 0.816 | * | * | * |
| CM5 | (480, 1, 2) | 0 | 2 | 4785 | 0.816 | * | * | * |



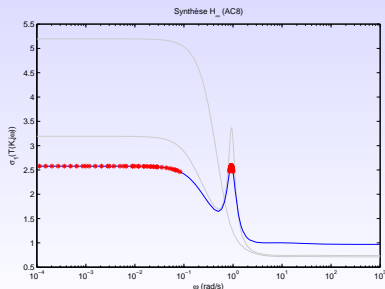
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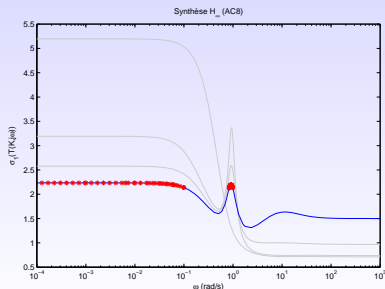
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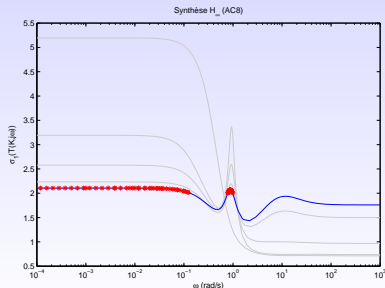
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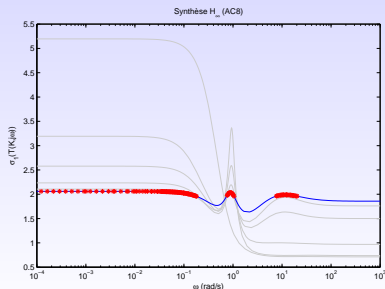
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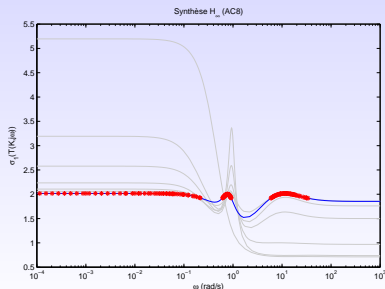
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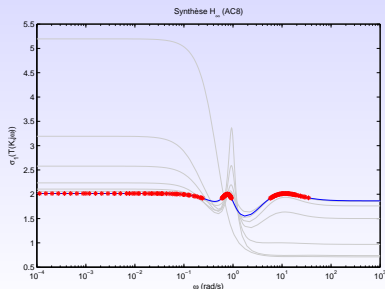
examples from Leibfritz's collection

| problem | (n, m, p) | order | iter | cpu (sec.) | nonsmooth H_∞ | H_∞ AL | FW | H_∞ full |
|---------|-------------|-------|------|------------|----------------------|---------------|-------|-----------------|
| AC8 | (9, 1, 5) | 0 | 20 | 45 | 2.005 | 2.02 | 2.612 | 1.62 |
| HE1 | (4, 2, 1) | 0 | 4 | 7 | 0.154 | 0.157 | 0.215 | 0.073 |
| REA2 | (4, 2, 2) | 0 | 31 | 51 | 1.192 | 1.155 | 1.263 | 1.141 |
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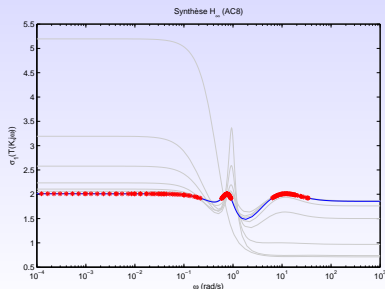
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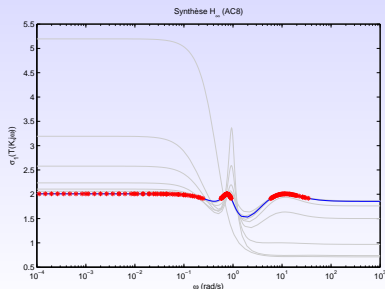
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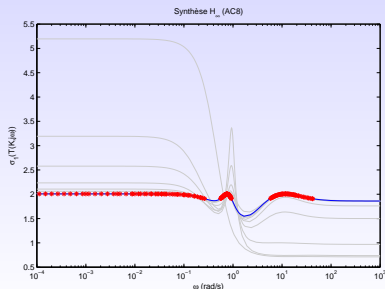
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time-domain design

$$\min_{K \in \mathcal{K}} \max_{t \in [0, +\infty]} \underbrace{\left\{ (z(K, t) - z_{max}(t))^+, (z_{min}(t) - z(K, t))^+ \right\}}_{= f_{\infty}(K)}$$

minimize maximum violation of SISO step response **envelope specification**

$$z_{min}(t) \leq z(K, t) \leq z_{max}(t)$$

- **stabilizing** initial controller K_0 .
- **simulate** step response for $t_l \in [0, T]$.
- **active times** (finite set) :

$$\hat{X}(K) = \left\{ t_l : z(K, t_l) - z_{max}(t) = f_{\infty}(K) \text{ or } z_{min}(t) - z(K, t_l) = f_{\infty}(K) \right\}$$

extended set $\hat{X}_e(K) \supset \hat{X}(K)$ with neighboring times.

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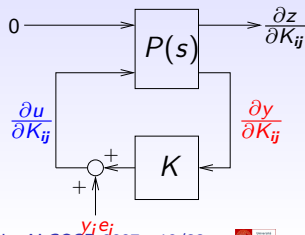
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simulated subgradients

$$\phi(K) = \sum_{t_l \in \hat{X}(K)} \pm \tau_l \left[\frac{\partial z}{\partial K_{ij}}(K, t_l) \right]_{i,j}$$

with $\tau_l \geq 0$ and $\sum_{t_l \in \hat{X}(K)} \tau_l = 1$



numerical results

2-DOF PID control of a SISO plant

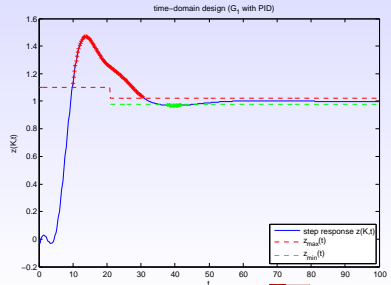
(4th-order)

t_s settling time at $\pm 2\%$

z_{OS} overshoot

| plant | contr. | t_s (s) | z_{OS} (%) |
|-------|--------|-----------|--------------|
| G_1 | ZN* | 46.22 | 46.92 |
| G_1 | IFT* | 21.34 | 5.37 |
| G_1 | NS | 20.94 | 1.95 |

* [Lequin et al., 03]



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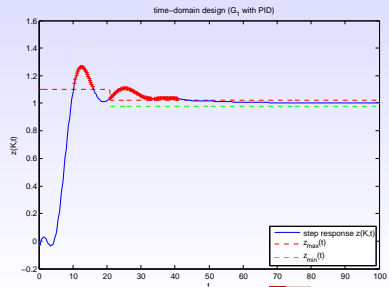
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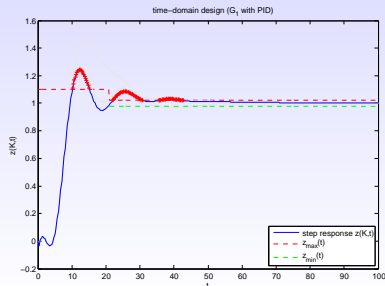
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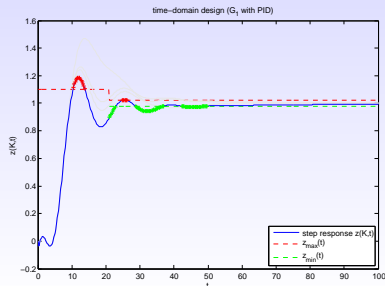
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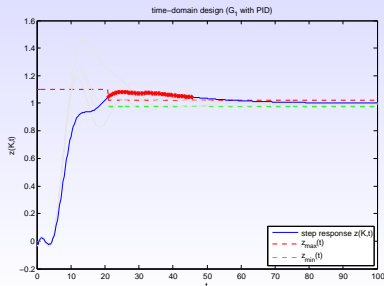
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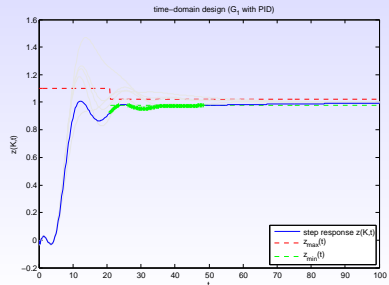
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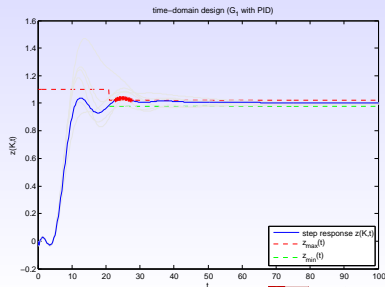
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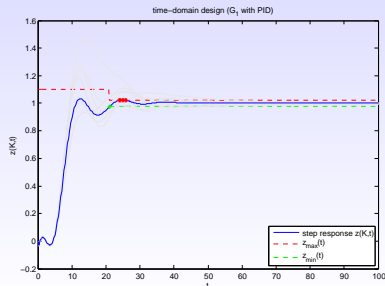
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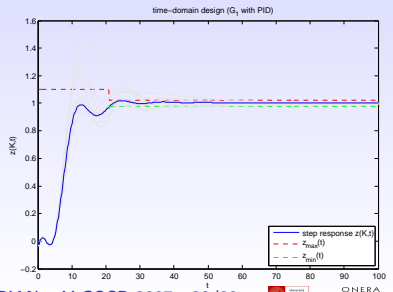
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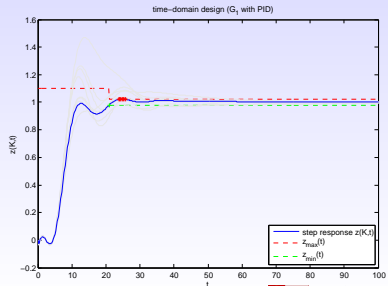
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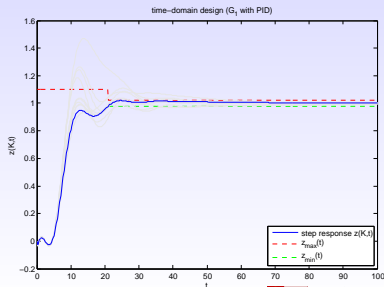
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